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# Hydrogen Absorption and Desorption Performance of Magnesium-Aluminium Alloys Produced by Powder Metallurgy

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(Received on 25th May 2013, accepted in revised form 19th September 2013)

**Summary:** The main scope of this study is investigating the hydrogen storage and desorption performance of Mg: Al (90:10),  $Mg_{17}Al_{12}$  and  $Mg_2Al_3$  alloys using a volumetric method. In the experiments, hydrogen pressure introduced into a reference volume was at approximately 20 Bar. Mg-Al alloys were prepared by a powder metallurgy technique. Pressing pressure levels of alloys were altered as 200, 400 and 600 MPa. Upon XRD patterns, after the pressing and sintering,  $\beta$ -Mg<sub>2</sub>Al<sub>3</sub> and Mg:Al(90:10) phases decomposed into  $\gamma$ -Mg<sub>17</sub>Al<sub>12</sub>, Mg and Al compositions.  $\gamma$ -Mg<sub>17</sub>Al<sub>12</sub> was the main phase in the hydrogen absorption/desorption process. The highest absorption of hydrogen was observed in the Mg:Al (90:10) alloys. The hydrogen desorption performance of the alloys decreased with the increase of absorption performance. Therefore the lowest desorption was observed in the Mg:Al (90:10) alloys.

Keywords: Metal alloys; Hydrogen storage and Desorption; powder metallurgy

# Introduction

Modern industrialised societies, which have had their economic growth based on the utilisation of energy locked in fossil fuels, can no longer ignore the effects of fossil fuels such as global warming, climate changes and natural disasters. The demand for energy continues to rapidly rise due to the continuing increase of the world population and the growing demand from developing countries to improve their living standards. The solution to this global energy problem need clean energy technologies. The development of efficient methods for hydrogen storage is a major issue that must be overcome in order to enable the use of hydrogen as an alternative energy carrier. The development of high capacity hydrogen storage materials that can be recharged under moderate conditions is a key barrier to the realisation of a hydrogen economy. Several studies report the development of hydrogen storage materials such as metal hydrides, carbon- based materials, chemical hydrides, boron compounds, etc. [1].

Among the known alloys with potential use in the hydrogen storage, Mg and Mg-based metallic hydrides are considered to be the most promising materials for hydrogen storage due to their high hydrogen capacity and low cost. Unfortunately, the practical applications are limited due to the poor absorption/desorption kinetics and high thermodynamic stability of these kinds of metal

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hydrides [2]. Therefore, various attempts have been made to reduce the thermodynamic stability, including alloying with transition or rare earth metals, adding fine oxide particles, adding halides, producing hydrides with a nano-crystalline structure, electrochemical hydriding and others [3].

To obtain the lightweight hydrogen storage alloy, element Al has been studied regarding its ability to interact with Mg as hydrogen storage material due to its low density and perfect thermal conductivity. Bouaricha et al. [4] reported the hydriding behaviour of Mg-Al and leached Mg-Al compounds prepared by high-energy ball milling. The measured hydrogen capacity of the milled material decreases with the Al content, from H/M=1.74 for pure un-milled Mg, to 1.38 for Mg:Al (90:10), and then to 1.05 for Mg:Al (75:25). Zaluska et al. [5] examined, with examples from a wide range of hydrides, the direct impact of the nano-scale structure, subsequent improvements in kinetics through nanoscale solid state catalysis, the special properties of nanocomposites, and the role played by nano-scale reactions. Their example of a functional nano-composite was that Mg-Al. Magnesium brings to the system high hydrogen capacity which, even after including the presence of Al, can reach 3.5-4.5wt. %. Aluminium provides improved heattransfer properties and modifies the hydrogenation thermodynamics in such a way that the system can operate at lower temperatures. Andreasen et al. [6] studied the interaction of hydrogen with an Mg-Al alloy pre-exposed to air with in situ time resolved Xray powder diffraction. The results showed that the addition of Al improved the resistance to oxygen contamination. Wang et al. [7] synthesised a composite containing Mg<sub>17</sub>Al<sub>12</sub> alloy and MgH<sub>2</sub> by ball milling. In comparison with the hydrogenation of Mg<sub>17</sub>Al<sub>12</sub> alloy and MgH<sub>2</sub>, the synergistic effect of ball-milled MgH<sub>2</sub> and Mg<sub>17</sub>Al<sub>12</sub> alloy on the hydrogen hydriding/dehydriding behaviour of the composite was discussed. Milanese et al. [8] have prepared nano-crystalline binary mixtures of Mg and nine different metals (Al, Cu, Fe, Mo, Mn, Sn, Ti, Zn and Zr) using mechanical alloying; their sorption capacities have been compared in order to study the effect of these additives as catalysing/destabilising

agents for Mg hydrogenation/ dehydrogenation. They found total H<sub>2</sub> intake and sorption efficiencies for compositions Mg 70% + Al 30%, Mg 55% +Al 45%, Mg 37% +Al 63%. For Mg-Al systems the general reaction scheme is:

 $Mg_nAl_m + nH_2 \leftrightarrow nMgH_2 + mAl$  (1)

For 70% Mg 30% Al alloy;

 $Mg_{17}Al_{12} + 9H_2 \leftrightarrow 4Mg_2Al_3 + 9MgH_2$  (2)

For 55% Mg 45% Al and 37% Mg 63% Al alloys;

$$Mg_{17}Al_{12} + 11H_2 \leftrightarrow 3Mg_2Al_3 + 11MgH_2 + 3Al$$
 (3)

These reactions are also expressed as follows for  $Mg_{17}Al_{12}$  [4, 9]. Initially, only  $Mg_{17}Al_{12}$  is decomposed to  $Mg_2Al_3$  and formed the  $MgH_2$ , and then  $Mg_2Al_3$  is reacted for the resulting  $MgH_2$ ;

$$Mg_{17}Al_{12}+(17-2y)H_2 \rightarrow yMg_2Al_3+(17-2y)MgH_2+(12-3y)Al$$
 (4)

$$Mg_2Al_3 + 2H_2 \rightarrow 2MgH_2 + 3Al \tag{5}$$

Crivello *et al.* [10] reported encouraging results for Mg–Al system with Nb<sub>2</sub>O<sub>5</sub> additive catalyst. Three nominal compositions [(Mg<sub>x</sub>Al<sub>100 - x</sub>)-99 + (Nb<sub>2</sub>O<sub>5</sub>) - 1 mol.%], X = 100 (Mg), X = 39 (β-Mg<sub>2</sub>Al<sub>3</sub>) and X = 70 (Mg +  $\gamma$ -Mg<sub>17</sub>Al<sub>12</sub>) have been investigated for their hydrogen equilibrium pressure of absorption and desorption reactions, from 250°C to 400°C. Glage *et al.* [11] presented a Powder Metallurgy (PM) route for the production of a hydrogen storage MgH<sub>2</sub>–Al composite material. Pure

aluminium specimens were sintered with two different sets of sintering parameters in order to investigate their effect on the properties of the matrix material after the sintering process. Next, a bulk composite consisting of MgH<sub>2</sub> and 20 wt.% Al was produced in order to evaluate the resistance to decrepitation. Tanniru et al. [12] evaluated the hydrogenation characteristics of an Mg-8at% Al alloy powder synthesised using the electro deposition technique to investigate the effect of Al addition on the stability of magnesium hydride. The characterization of the hydrogenation behaviour within the 180°C-280°C temperature range and the subsequent micro structural analysis elucidated that the amount of Al present in the hydride decreased with the increasing temperature. Hydrogenation properties and mechanical stability of pellets made starting from compressed ball-milled MgH<sub>2</sub> powders mixed with catalysts (Nb<sub>2</sub>O<sub>5</sub> and graphite) and a binding agent (aluminium powder) have been investigated by Khandelwal et al. [13]. The best cycling behaviour and mechanical strength stability have been observed for pellets of catalysed MgH<sub>2</sub> powders added with 5 wt% aluminium annealed in a vacuum at 450°C before starting the a/d cycles. Kalisvaart et al. [14] focused on the hydrogen sorption properties of 1.5mm thick Mg-based films with Al, Fe and Ti as alloying elements. The binary alloys are used to establish a baseline case for the ternary Mg-Al-Ti, Mg-Fe-Ti and Mg-Al-Fe compositions. They show that the ternary alloys in particular display remarkable sorption behaviour at 200 °C the films are capable of absorbing 4-6 wt% hydrogen in seconds, and desorbing in minutes.

The main scope of this study is to investigate the  $H_2$  absorption and desorption performance of Mg:Al (90:10), Mg<sub>17</sub>Al<sub>12</sub> and Mg<sub>2</sub>Al<sub>3</sub> alloys, produced in different press and sintering conditions, using a volumetric method.

#### Results

#### Physical Characterization of Materials

In order to define the formation of phases in the alloys, a Rigaku XRD diffractometer was used. The X-ray analysis was operated at 30 kV, 30 mA with Cu K $\alpha$  radiation. XRD results confirmed the presence of crystalline phases, Mg, Al, Mg<sub>2</sub>Al<sub>3</sub>, Mg<sub>17</sub>Al<sub>12</sub>, MgAl<sub>2</sub>O<sub>4</sub>, see Figs. 1-3.



Fig. 2: XRD patterns of Mg<sub>17</sub>Al<sub>12</sub> alloys.



Fig. 3: XRD patterns of Mg:Al (90:10) alloys.

## Hydrogen Absorption and Desorption

The hydrogen storage performance of the Mg-Al alloys is mainly denoted by the hydrogen absorption and desorption capacity.

- The effect of the alloy types and pressing conditions for hydrogen absorption and desorption are presented in Fig. 4 and Fig. 5, respectively.
- It was obtained from the XRD patterns of Mg<sub>17</sub>Al<sub>12</sub> alloy that the phase of 600MPa Mg<sub>17</sub>Al<sub>12</sub> was a pure phase. Therefore, the hydrogen absorption ratio of this alloy was the highest (Fig. 4).
- The existence of Mg<sub>2</sub>Al<sub>3</sub> decreased the hydrogen absorption. It is shown in Fig. 4 that absorbed H<sub>2</sub> weight of 200 and 400MPa Mg<sub>17</sub>Al<sub>12</sub> alloys were lower than 600MPa Mg<sub>17</sub>Al<sub>12</sub>, because of existing of Mg<sub>2</sub>Al<sub>3</sub> (XRD patterns of Mg<sub>17</sub>Al<sub>12</sub> presented in Fig. 2).
- The porosities of 600MPa Mg<sub>17</sub>Al<sub>12</sub> and 400MPa Mg:Al(90:10) were the same value of 76.4. Therefore, as seen in Fig. 4 and Fig. 5, their hydrogen absorption and desorption characteristics were the same.
- According to the Mg-Al binary phase diagram, higher Mg concentration led to the formation of 2-phases compound; composed Mg- phase and γ-Mg<sub>17</sub>Al<sub>12</sub> phases. According to the XRD data, it can be clearly seen that Mg rich Mg;Al (90:10)

phase was transformed into the  $\gamma$ -Mg<sub>17</sub>Al<sub>12</sub> and Mg phases. Comparing all alloys with XRD patterns, the maximum amount of the  $\gamma$ -Mg<sub>17</sub>Al<sub>12</sub> phase and the maximum hydrogen absorption were managed with Mg:Al (90:10) alloys.

- From the XRD results, Al in the alloys of Mg<sub>2</sub>Al<sub>3</sub> and Mg<sub>17</sub>Al<sub>12</sub> dissolved under pressure and the weight of Al increased in the phases with increasing pressure (Fig. 1 and Fig. 2). The hydrogen desorption performance of the alloys decreased with the increasing Al content (Fig. 5). Dai *et al.* [15] studied the Al, Ti, Mn, and Ni doped MgH<sub>2</sub> systems and found that adding Al marginally increases the dehydrogenation energy.
- The formation of MgAl<sub>2</sub>O<sub>4</sub> was observed in Mg<sub>2</sub>Al<sub>3</sub> phase from XRD patterns of Fig. 1. In this phase Al formation was restricted because of the contribution of oxidized species to slow the kinetics of Al dissolution. Therefore dehydrogenation efficiency of 400MPa Mg<sub>2</sub>Al<sub>3</sub> was better than 200MPa Mg<sub>2</sub>Al<sub>3</sub> due to the deficiency of Al.
- The lowest absorption and the highest desorption values of hydrogen were received from Mg<sub>2</sub>Al<sub>3</sub> and Mg<sub>17</sub>Al<sub>12</sub> alloys which were pressed at 200MPa. These alloys had the same pure Mg<sub>2</sub>Al<sub>3</sub> phase (Fig. 1 and 2).
- It can be clearly seen from Table-1 and Fig. 5 that the Mg<sub>2</sub>Al<sub>3</sub>, Mg<sub>17</sub>Al<sub>12</sub> and Mg:Al (90:10) alloys pressed at 200 MPa had larger porosity

and higher desorption values than the other alloys which were exposed to different pressures. Due to its small molecular structure, hydrogen has a high leakage capability. The pores of the alloys facilitated dehydrogenation.

Table-1: Pressing pressures and porosity values of alloys.

Alloy	Pressing Pressure (MPa)	Porosity (%)
37% Mg -63%Al(Mg <sub>2</sub> Al <sub>3</sub> )	200	82.2156
	400	78.2085
	600	78.5822
47% Mg -53%Al(Mg <sub>17</sub> Al <sub>12</sub> )	200	78.6819
	400	77.3982
	600	76.4945
90% Mg -10%Al	200	80.074
	400	76.3531
	600	76.0325



Fig. 4: Hydrogen absorption performances of alloys.



Fig. 5: % Hydrogen amounts (desorbed hydrogen/ absorbed hydrogen, w/w).

## Experimental

Mg- Al alloys were prepared by a powder metallurgy technique which has been explained in a previous study [16]. Mg (99.8 wt.%) and Al powders (99.8 wt.%) with an average size of  $-44 \,\mu\text{m}$  (Alfa Aesar) were mixed and blended in a rotating container for 12 hours to create a homogenous mixture. The blended powder was then cold-pressed

into a cylindrical sample with a diameter of 10mm and a height of 10-20 mm at compaction pressure levels of 200, 400 and 600MPa. The powder compact was then loaded into a furnace and heated to 400°C under an argon atmosphere and sintered for approximately 4 hours.

The general porosity of the specimens was calculated using the formula;

$$\varepsilon = \left(1 - \frac{\rho}{\rho_0}\right) x 100 \tag{6}$$

In which  $\rho$  and  $\rho_0$  are the density of the specimen and its corresponding theoretical density, respectively. Pressing pressures and porosity values of alloys are presented in Table-1.

Fig. 6 shows the schematic diagram of the experimental apparatus. A volumetric method was applied to the measurement of absorption and desorption of  $H_2$ . The system consisted of a sample container and a reference volume made from stainless steel, a digital manometer attached to a reference volume, piping, vacuum pump and a burette inserted upside down to measure the volume  $H_2$ .



Fig. 6: Schematic diagram of the experimental apparatus.

#### Absorption

The experimental procedures for absorption measurements are as follows:

1- In order to allow the sample to reach its best sorption performance the samples were placed in an  $H_2$  atmosphere at 35 bar for 24 hours. This activation procedure was repeated five times.

- 2- The sample was charged into the sample container and the system was closed. A vacuum pump was operated continuously for 15 minutes.
- 3- The experimental apparatus was isolated from the vacuum system by closing the isolation valve. In addition, the sample container was isolated using the sample isolation valve.
- 4- H<sub>2</sub> gas was introduced into the reference volume and the pressure was recorded. Approximately 20 bar was the supply pressure of the reference volume.
- 5- The sample isolation valve was opened in order to start absorption. The system pressure change was recorded.
- 6- The sample container was heated to 80°C (2°C/minute) gradually and maintained at this temperature for 260 minutes.
- 7- After 5 hours, the sample container was cooled to room temperature to lock H<sub>2</sub> in the crystal lattice of the alloys. The sample isolation valve was closed again and the needle valve, which was inserted between the sample container and burette, was opened to measure the H<sub>2</sub> volume.
- 8- The sample container was discharged and isolated once again, and the procedure was returned to 2. Next, procedures 2-7 were repeated and the  $H_2$  volume of the empty sample container was measured.
- 9- The absorbed amount of  $H_2$  was calculated from the difference of measured volumes at 7 and 8.

Similar systems were used by Langohr *et al.* [17], Kawamura *et al.* [18], Muthukumar *et al.* [19].

The system pressure change was recorded during absorption experiments. An example of these records can be found in Fig. 7. For all samples the system pressure was attained to a certain pressure at approximately 260 minutes. Therefore, the absorption experiments were limited to 5 hours. Experiments were repeated twice.

# Desorption

For all samples, the hydrogen release processes were performed at the temperature of 100°C and open to atmospheric pressure. The experimental procedures for desorption measurements are as follows:

1- After the absorption process, the sample container was isolated using the sample isolation valve. Then the needle valve, which was inserted between the sample container and the burette, was opened to measure the H<sub>2</sub> volume.

- 2- The sample container was gradually heated to 100°C (2°C/minute).
- 3- The system pressure change was recorded.
- 4- The releasing  $H_2$  volume was recorded.
- 5- Procedures 1-5 were repeated and the H<sub>2</sub> volume of the empty sample container was measured once again.
- 6- The desorbed amount of  $H_2$  was calculated from the difference of the measured volumes at 4 and 5.



Fig. 7: System pressure change during the absorption experiment of  $Mg_{17}Al_{12}$  pressed at 600MPa.

## Conclusions

In this study three Mg-Al alloys; Al rich β- $Mg_2Al_3$ ,  $\gamma$ - $Mg_{17}Al_{12}$  and Mg rich Mg:Al (90:10) phases were tested for hydrogen storage and desorption. Performance studies were carried out by varying the alloy types and the pressing pressure levels of alloys. The composition of the alloys was changed during the pressing and sintering procedures. Upon XRD patterns, after the pressing and sintering,  $\beta$ -Mg<sub>2</sub>Al<sub>3</sub> and Mg:Al (90:10) phases decomposed into y-Mg17Al12, Mg and Al compositions. y-Mg<sub>17</sub>Al<sub>12</sub> was the main phase in the hydrogen adsorption/desorption process. Mg<sub>2</sub>Al<sub>3</sub> alloy (pressed at 600MPa) stored approximately 0.37 wt.% hydrogen, while 200MPa stored 0.15 wt.% hydrogen. Pressing pressure levels and also the pore sizes of alloys had a significant effect on the absorption and desorption performance of hydrogen. Beside these, the addition of Al effected the dehydrogenation of alloys negatively due to its positive effect on the dehydrogenation energy.

#### Acknowledgements

The financial support that was provided by Atatürk University (AÜ BAP 2007/139) is gratefully acknowledged.

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